PART COOPERATION TREAT

	From the INTERNATIONAL BUREAU		
PCT	То:		
NOTIFICATION OF ELECTION (PCT Rule 61.2)	Assistant Commissioner for Patents United States Patent and Trademark Office Box PCT Washington, D.C.20231 ETATS-UNIS D'AMERIQUE		
Date of mailing (day/month/year)			
29 August 2000 (29.08.00)	in its capacity as elected Office		
International application No. PCT/SE99/02300	Applicant's or agent's file reference PCT 51259 si		
International filing date (day/month/year)	Priority date (day/month/year)		
08 December 1999 (08.12.99)	11 December 1998 (11.12.98)		
Applicant			
DAHLBÄCK, Mats et al			
The designated Office is hereby notified of its election made in the demand filed with the International Preliminary 07 July 2000 (0) in a notice effecting later election filed with the International Preliminary 7. The election was was not made before the expiration of 19 months from the priority of Rule 32.2(b).	Examining Authority on: 17.07.00) ational Bureau on:		
	Authorized officer		

Facsimile No.: (41-22) 740.14.35

The International Bureau of WIPO 34, chemin des Colombettes 1211 Geneva 20, Switzerland

Manu Berrod

Telephone No.: (41-22) 338.83.38

PATENT COOPERATION TREATY

PCT

INTERNATIONAL-TYPE SEARCH REPORT

(PCT Article 15.5)

National application No. 9804292-2	Country or Office of	f filing	Applicant's or agent's file reference SE 400 036 OF	
Filing date (day/month/year)		(Earliest) Priority	Date (day/month/year)	
11 December 1998				
Applicant			·	
Asea Brown Boveri AB				
		International type	search request No.	
Date of request for international-type se	earcn	ļ	search request 140.	
11 December 1998		SE 98/01421		
This international-type search report he to the applicant. This international-type search report of X lt is also accompanied by a companied	consists of a total of	2 sheets.		
1. Certain claims were found un	searchable (See Box 1	I).		
2. Unity of invention is lacking	(See Box II).			
3. The international application international-type search was	n contains disclosure of carried out on the b	of a nucleotide and/ asis of the sequence	or amino acid sequence listing and the e listing	
l u	ed with the internation	nal application.		
fu	rnished by the applica	ant separately from	the international application,	
	but not acco	ompanied by a state g beyond the disclo	ement to the effect that it did not include sure in the international application as filed.	
tr.	anscribed by this Aut	hority.		
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INTERNATIONAL PRELIMINARY EXAMINATION REPORT

FOT

(PCT Article 36 and Rule 70)

Applicant's or agent's file reference PCT 51259 si/ak	FOR FURTHER ACTION	TION See Notification of Transmittal of International Preliminary Examination Report (Form PCT/IPEA/4)				
International application No.	International filing date (da	day/month/year) Priority date (day/month/year)				
PCT/SE99/02300	phreation to.					
International Patent Classification (IPC) o	<u> </u>	IPC2				
C 22 C 16/00, G 21 C		L C /				
C 22 C 18/00, G 21 C	3/02					
Applicant		-				
ABB Atom AB et al						
This international preliminary exa Authority and is transmitted to the	amination report has been properties applicant according to Art	epared by this Inter icle 36.	national Preliminary Examining			
2. This REPORT consists of a total	of 4 sheets, i	ncluding this cover	sheet.			
			ion, claims and/or drawings which have			
been amended and are the	basis for this report and/or slow 607 of the Administrative	heets containing rec	tifications made before this Authority			
These annexes consist of a total	of sheets.					
3. This report contains indications relating to the following items:						
Basis of the report						
II Priority						
Non-establishment of opinion with regard to novelty, inventive step and industrial applicability						
IV Lack of unity of invention						
V Reasoned statement citations and explan	V Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement					
VI Certain documents	cited					
VII Certain defects in the	ne international application					
VIII Certain observations on the international application						
Date of submission of the demand Date of completion of this report						
Date of submission of the demand Date of completion of this report						
07.07.2000		30.11.200	0			
Name and mailing address of the IPEA/s	SE	Authorized officer				
Patent- och registreringsverke Box 5055	t Telex 17978					
S-102 42 STOCKHOLM	PATOREG-S	Nils Engn				
Facsimile No. 08-667 72 88		Telephone No. 08	I-182 25 00			



Into	nal application No.	
nom /9	E99/02300	
PC173	10007	

## With regard to the elements of the international application.* The description:	INTERNATIONAL PRELIMINARY EXAMINATION REZ	PCI7BET
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the claims, Nos. the drawings, sheet/fig the drawings, sheet/fig This report has been established as if (some of) the amendments had not been made, since they have been beyond the disclosure as filed, as indicated in the Supplemental Box (Rule 70.2 (c)).** * Replacement sheets which have been furnished to the receiving Office in response to an invitation under Article Replacement sheets which have been furnished to the receiving Office in response to an invitation under Article Replacement sheets which have been furnished to this report since they do not contain amendments (Rule in this report as "originally filed" and are annexed to this report to under item I and annexed to this report as "originally filed" and are unusually be referred to under item I and annexed to this report as "originally filed" and are unusually to the amendments had not been made, since they have been function to the supplemental Box (Rule 70.2 (c)).**	the language of a translation of the international application the language of publication of the international application or 55.3). 3. With regard to any nucleotide and/or amino acid sequence dispreliminary examination was carried out on the basis of the sequence of	amendments had not been made, since they have been considered

V.	Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability;
	citations and explanations supporting such statement

1	Statement

Novelty (N)	Claims Claims	1-12	YES NO
Inventive step (IS)	Claims Claims	1-12	YES NO
Industrial applicability (IA)	Claims Claims	1-12	YES NO

2. Citations and explanations (Rule 70.7)

The Invention

The invention relates to a zirconium alloy for uses in nuclear plants. The main alloying elements are Nb 0.5-1.6%, Sn 0.5-0.85% and Fe 0.3-0.6%. Optionally, the alloy contains Ni <0.2% and Cr <0.6%. The alloy is optimised with respect to physical, mechanical and corrosion properties.

Documents cited in the International Search Report.

- D1 US 5 560 790 A
- D2 WO 94/14 990 A1
- D3 Isobe T. et.al. "Development of Highly Corrosion Resistant Zirconium-Base Alloys", ASTM Publication STP 1132, Zirconium in the Nuclear Industry: Ninth International Symposium, Philadelphia 1991, pp. 246-367. p. 348-p. 353, p. 361-p. 366.

Discussion

The documents were cited to define the general state of the art not considered to be of particular relevance.

In D1 a zirconium alloy comprising Nb 0.5-2.0%, Sn 0.7-1.5% and at least one of Fe, Ni and Cr 0.07-0.28% is referred to as state of the art that. This alloy has not satisfactory corrosion properties, not even with a content of 0.3-0.6% Fe (col. 2, 1 12 -. col. 3, 1 21). This later composition includes the alloy according to present claims. The alloy disclosed in D1 comprises Nb 0.5-1.5%, Sn 0.9-1.5% and Fe 0.3-0.6% (col. 4, 1 13-1 67). The present alloy differs from this

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nal application No. PCT/SE99/02300

(To be used when the space in any of the preceding boxes is not sufficient)

in that the content of Sn is reduced. In D1 the examples Continuation of: V indicate that increasing Sn contents increase the corrosion

D2 discloses a zirconium alloy comprising Sn 0.45-0.75%, Fe 0.4-0-53, Cr 0.2-0.3% and Nb 0.3-0.5%. It is stated that the relatively low contents of Sn and Nb improve the corrosion resistance, (p 6, 1 16- p 7, 1 5 and p 8 11. 7-20). This is contradictory to what is stated in D1.

In the paper D3 the effects of Nb, Sn and Fe on strength and corrosion properties of zirconium alloys are discussed. From fig 2 and 3 it can be concluded that for contents of Nb according to the present claims the content of Sn should be with regard to corrosion properties. However, 358 mechanical properties are degraded (p. 353 and p. alloy compositions tested according to the diagrams all contain 0.2% Fe, but can be "Conclusions"). increased to improve the tensile strength without affecting the corrosion resistance.

Therefore, the alloy according to present claims is novel. The Conclusion statements in D1, D2 and D3 about effects, especially combined effects, of the alloying elements do not clearly indicate that the selected contents of the alloying elements in the present alloy is optimal. Consequently, the alloy according to present claims is not considered to be obvious to a person skilled in the art.

PCT

REQUEST

The undersigned requests that the present international application be processed according to the Patent Cooperation Treaty.

For receiving Office use only	
International Application No.	
International Filing Date	
Name of receiving Office and "PCT International Application"	

•					
	Applicant's or agent's file reference				
<u></u>	(if desired) (12 characters maximum) PCT 51259 si/cg				
Box No. I TITLE OF INVENTION	•				
"Zirconium based alloy and compon	ent in a nuclear onewer along				
	ent in a nuclear energy plant"				
Box No. II APPLICANT					
Name and address: (Family name followed by given name: for a	egal enting full official				
Name and address: (Family name followed by given name: for a designation. The address must include postal code and name of cou address indicated in this Box is the applicant's State (that is, country of residence is indicated below.)	ntry. The country of the person is also inventor. This person is also inventor.				
of residence is indicated below.)					
	Telephone No.				
ABB AB					
SE-721 83 Västerås	Facsimile No.				
SWEDEN .					
	Teleprinter No.				
State (that is, country) of nationality:	State (that is. country) of residence:				
Sweden	Sweden				
This person is applicant all designated all designated	States except the United States the States indicated in				
	ates of America of America only the Supplemental Box				
Box No. III FURTHER APPLICANT(S) AND/OR (FURTH	HER) INVENTOR(S)				
Name and address: (Family name followed by given name: for a l	agal ansing full official				
Name and address: (Family name followed by given name: for a l designation. The address must include postal code and name of cour	niry. The country of the This person is:				
address indicated in this Box is the applicant's State (that is, country, of residence is indicated below.)	of residence if no State				
of residence is indicated below.)	applicant only				
DAHLBÄCK, Mats	x applicant and inventor				
Mangelgatan 13					
SE-724 76 Västerås	inventor only (If this check-box				
SWEDEN	is marked, do not fill in below.)				
State (that is, country) of nationality:	1 State (that is a second of side				
Sweden	State (that is, country) of residence:				
	Sweden				
This person is applicant all designated all designated for the purposes of:	1 States except x the United States the States indicated in ates of America only the Supplemental Box				
x Further applicants and/or (further) inventors are indicated o	n a continuation sheet.				
Box No. IV AGENT OR COMMON REPRESENTATIVE; OR ADDRESS FOR CORRESPONDENCE					
The person identified below is hereby/has been appointed to act o of the applicant(s) before the competent International Authorities	n behalf X agent common representative				
Name and address: (Family name followed by given name: for a designation. The address must include postal co	legal entity, full official Telephone No.				
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BERGLUND, Stefan; ISRAELSSON, S	tefan; Facsimile No.				
BJERKÉN, Håkan; FRÖDERBERG, Osk	ar; or				
OLSSON, Jan;	08 - 663 02 60				
Östermalmsgatan 58	Teleprinter No.				
SE-114 50 Štockholm, SWEDEN					
Address for correspondences Made this short by					
space above is used instead to indicate a special address to w	to agent or common representative is/has been appointed and the				

State (that is, country) of residence:

the United States

of America only

all designated States except the United States of America

Further applicants and/or (further) inventors are indicated on another continuation sheet.

Form PCT/RO/101 (continuation sheet) (July 1998)

all designated

State (that is, country) of nationality:

This person is applicant

for the purposes of:

the States indicated in

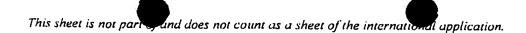
the Supplemental Box

Sheet No. . 3....

L	Box A	io.V						
	The following designations are hereby made under Rule 4.9(a) (mark the applicable check-boxes: at least one must be marked):							
	Regional Patent							
		AP	ARIPO Patent: GH Ghana, GM Gambia, KE Kenya, LS Lesotho, MW Malawi, SD Sudan, SZ Swaziland, UG Uganda, ZW Zimbabwe, and any other State which is a Contracting State of the Harare Protocol and of the PCT					
		E.A	Eurasian Patent: AM Armenia, AZ Azerbaijan, BY Belarus, KG Kyrgyzstan, KZ Kazakhstan, MD Republic of Moldova, RU Russian Federation, TJ Tajikistan, TM Turkmenistan, and any other State which is a Contracting State of the Eurasian Patent Convention and of the PCT					
	図	EP	European Patent: AT Austria BE Belgium. CH and LI Switzerland and Liechtenstein. CY Cyprus. DE Germany. DK Denmark. ES Spain. FI Finland. FR France. GB United Kingdom. GR Greece. IE Ireland. IT Italy. LU Luxembourg. MC Monaco. NL Netherlands. PT Portugal. SE Sweden. and any other State which is a Contracting State of the European Patent Convention and of the PCT					
		OA OAPI Patent: BF Burkina Faso. BJ Benin. CF Central African Republic. CG Congo. CI Côte d'Ivoire. CM Cameroon. GA Gabon. GN Guinea. ML Mali. MR Mauritania. NE Niger. SN Senegal. TD Chad. TG Togo. and any other State which is a member State of OAPI and a Contracting State of the PCT infother kind of protection or treatment desired. specify on dotted line)						
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Precautionary Designation Statement: In addition to the designations made above, the applicant also makes under Rule 4.9(b) all other designations which would be permitted under the PCT except any designation(s) indicated in the Supplemental Box as being excluded from the scope of this statement. The applicant declares that those additional designations are subject to confirmation and that any designation which is not confirmed before the expiration of 15 months from the priority date is to be regarded as withdrawn by the applicant at the expiration of that time limit. (Confirmation of a designation consists of the filing of a notice specifying that designation and the payment of the designation and confirmation fees. Confirmation must reach the receiving Office within the 15-month time limit.)

	_ 🌥	Sheet No 4					
Box No. VI PRIORITY C	LAIM	Further prior	prity claims are indicated	in the Supplemental Box			
Filing date	Number	i	Where earlier applicati				
of earlier application (day/month/year)	of earlier application	national application:	regional application:*	international application:			
item (1)		country	regional Office	receiving Office			
11/12/1998	9804292-2	Sweden					
item (2)			·				
item (3)	·						
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Where the earlier application is	am 10/00 11- 11- 11-	is the receiving Office) identifi	. ` . —	(1)			
			ed (Rule 4.10(b)(ii)). See S	ie country party to the Paris upplemental Box.			
BOX : 40. VII INTERNATIO	NAL SEARCHING A	UTHORITY					
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competent to carry out the internal the Authority chosen; the two-lette	tional search, indicate	Date (day/month/year)					
ISA / SE			0 /01 401	Country (or regional Office)			
Box No. VIII CHECK LIST			98/01421	Sweden			
This international application co							
the following number of sheets	8: 1	tional application is accompani dculation sheet	ied by the item(s) market	i below:			
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description (excluding sequence listing part)		ate signed power of attorney					
claims .		of general power of attorney;					
2 - Statement explaining lack of signature							
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sequence listing and (language):							
7. separate indications concerning deposited microorganism or other biological material 8. nucleotide and/or amino acid sequence listing in computer readable form							
Total number of sheets:	16 9. 🔀 other	(specify): ITS-report	ice nating in computer re-	adable form			
Figure of the drawings which		Language of filing of the		···			
should accompany the abstract:		international application:	Swedish				
	OF APPLICANT OR		Ÿ				
Next to each signature, indicate the nar	me of the person signing and	d the capacity in which the person sig	rs (if such capacity is not obvi	ious from reading the request).			
Stockho	olm, 7 Decem	ber 1999					
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	Fo	or receiving Office use only -					
1. Date of actual receipt of the international application:	purported			2. Drawings:			
3. Corrected date of actual rece	int due to later but		· .				
timely received papers or dra the purported international a	awings completing			received:			
4. Date of timely receipt of the corrections under PCT Artic	required le 11(2):			not received:			
5. International Searching Auth (if two or more are competen	ority nt): ISA /	6. Transmitta until search	l of search copy delayed n fee is paid.				
Date of receipt of the record cop by the International Bureau:	Py For I	nternational Bureau use only					



PCT For receiving Office use only FEE CALCULATION SHEET International application No. Annex to the Request Applicant's or agent's tile reference Date stamp of the receiving Office PCT 51259 si/cg Applicant ABB AB et al CALCULATION OF PRESCRIBED FEES 2. SEARCH FEE . 510: S International search to be carried out by (If two or more International Searching Authorities are competent in relation to the international application, indicate the name of the Authority which is chosen to carry out the international search.) 3. INTERNATIONAL FEE Basic Fee The international application contains 16 sheets. 3 500:additional amount Add amounts entered at b1 and b2 and enter total at B . **Designation Fees** The international application contains 4 designations. D 800:-200:number of designation fees amount of designation fee payable (maximum 10) 6 700:-1 Add amounts entered at B and D and enter total at I . . (Applicants from certain States are entitled to a reduction of 75% of the international fee. Where the applicant is (or all applicants are) so entitled, the total to be entered at I is 25% of the sum of the amounts entered at B and D.) 4. FEE FOR PRIORITY DOCUMENT (if applicable) P 5. TOTAL FEES PAYABLE. 16 210:-Add amounts entered at T. S, I and P, and enter total in the TOTAL box TOTAL The designation fees are not paid at this time. MODE OF PAYMENT authorization to charge bank draft coupons deposit account (see below) cheque cash other (specify): postal money order revenue stamps DEPOSIT ACCOUNT AUTHORIZATION (this mode of payment may not be available at all receiving Offices) The RO/ is hereby authorized to charge the total fees indicated above to my deposit account. (this check-box may be marked only if the conditions for deposit accounts of the receiving Office so permit) is hereby authorized to charge any deficiency or credit any overpayment in the total fees indicated above to my deposit account. is hereby authorized to charge the fee for preparation and transmittal of the priority document to the International Bureau of WIPO to my deposit account. Deposit Account No. Date (davimonth/year) Signature

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with the	one chosen by the applicant. The	fur same or two-letter code of that same

SE IPEA/

CHAPTER II

DEMAND

under Article 31 of the Patent Cooperation Treaty:

The undersigned requests that the international application specified below be the subject of international preliminary examination according to the Patent Cooperation Treaty and hereby elects all eligible States (except where otherwise indicated).

For	International Preliminary Examining Authorit	y use only
	Date of receipt of I	DEMAND
entification of IPEA	THE INTERNATIONAL APPLICATION	Applicant's or agent's file reference PCT 51259 si/ak
nternational application No.	International filing date (day/month/year) 8/12/99 and component in a nuclear ene	(Earliest) Priority date (day/month/year) 11/12/98
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Sheet No. . 4

International application No. PCT/SE99/02300

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CHAPTER II

PCT

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(54) Title: ZIRCONIUM BASED ALLOY AND COMPONENT IN A NUCLEAR ENERGY PLANT

(57) Abstract

A zirconium-based alloy, suitable for use in a corrosive environment, where it is subjected to increased radiation and comprises 0.5-1.6 percentage by weight Nb and 0.3-0.6 percentage by weight Fe. The alloy is characterised in that it comprises 0.5-0.85 percentage by weight Sn.

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WO 00/36170 PCT/SE99/02300

Zirconium-based alloy and component in a nuclear energy plant

BACKGROUND OF THE INVENTION AND PRIOR ART

The present invention concerns a zirconium-based alloy, suitable for use in a corrosive environment where it is subjected to increased radiation and comprising 0.5-1.6 percentage by weight Nb and 0.3-0.6 percentage by weight Fe. The invention also concerns a component in a nuclear energy plant, which comprises an alloy of the mentioned kind.

According to the prior art it is known to provide, in a nuclear energy plant, a component which comprises a zirconium-based alloy of the above-mentioned kind. Such an alloy has the advantage of fulfilling the requirements which are demanded on mechanical as well as corrosion properties of a material which in a corrosive environment is subjected to an increased radiation, in particular neutron radiation of the fast neutron kind.

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Thanks to its relatively high Fe-content it is possible through a suitable heat treatment, comprising annealing and quenching, to obtain secondary phase particles consisting of Zr, Fe and Nb in a matrix of α -phase of the zirconium-based alloy. By a suitable choice of the heat treatment variables time and temperature it is furthermore, with given contents of the included alloying materials Nb and Fe, possible to control the size of and the distribution of the secondary phase particles. The secondary phase particles may have a positive effect on the corrosion resistance of the alloy. It is therefore important to optimize the distribution of and

the size of the existing secondary phase particles. It is thereby highly important to find a suitable composition of the alloying elements included in the alloy.

The document US 5 560 790 describes a zirconium-based alloy 5 which comprises 0.5-1.5 percentage by weight Nb, 0.9-1.5percentage by weight Sn and 0.3-0.6 percentage by weight Fe. Furthermore, this alloy comprises 0.005-0.2 percentage by weight Cr, 0.005-0.04 percentage by weight C, 0.05-0.15 percentage by weight O, 0.005-0.15 percentage by weight Si 10 and the rest Zr. Thereby a microstructure is achieved in the material which includes particles of the kind $Zr(Nb,Fe)_2$, Zr(Nb,Cr,Fe) and $(Zr,Nb)_3Fe$. These secondary phase particles give the material good corrosion properties and 15 mechanical properties. Thanks to the high Fe-content. precipations of $\beta\text{-Nb-phase}$ are avoided, which would have a negative influence on the resistance of the material against local corrosion attacks.

Sn is said to have a high solubility in the lpha-phase and will 20 therefore, when it is present to the given amount, be dissolved in the α -phase and contribute to improved corrosion properties and mechanical properties of the same. It is pointed out that a too low content of Sn (below 0.9 percentage by weight) in the material influences the tensile 25 strength of the material both in the long and in the short term. Furthermore, such a low Sn-content suppresses to a smaller extent a negative effect of a possible nitrogen incorporation on the corrosion resistance of the material. A Sn content above 1.5 percentage by weight influences the 30 susceptibility of the material to working and in particular to cold working.

It is mentioned that Si and C contribute to a reduction of the size of the particles and to bring about a structural homogeneity in the material.

Oxygen is said to contribute to a finer structure of the material and is also used as a means for reinforcing the material through the solid solution, a so-called "solid solution strengthener".

Nb is said to contribute to the strength properties of Zr and increases the corrosion resistance of the alloy by forming secondary phase particles together with Zr and Fe.

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It is furthermore pointed out that with a Nb-content below 0.5 percentage by weight of the material, a Fe-content below 0.3 percentage by weight and a Cr-content below 0.005 percentage by weight, the total portion of secondary phase particles of the above-mentioned kind in the $\alpha\text{-zirconium}$ matrix of the end product is considerably lower than 60 percentage by volume of the total amount of iron-containing secondary phase particles, which results in that negatively is material the resistance of corrosion influenced. With a Nb-content above 1.5 percentage by weight, a large number of large particles of $\beta ext{-Nb}$ phase are 20 formed in the material, which also reduces the corrosion resistance of the same.

It is also mentioned that a Cr-content above 0.2 percentage 25 the formation in may result weight intermetallic compounds of Zr-Cr, which has an opposite i.e. negative, influence on the workability and the tensile strength of the material.

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SUMMARY OF THE INVENTION

A purpose with the present invention is to provide a zirconium-based alloy with such a composition that the distribution of and the size of secondary phase particles in the alloy, the kind of secondary phase particles and the 35

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content of different alloying elements in the α -phase of the alloy are such that the alloy is optimized with respect to physical and mechanical properties as well as corrosion properties. In particular, these properties should be optimized with respect to an application where the alloy is subjected to an increased radiation of the fast-neutron kind in a corrosive environment, such as in the reactor core of a nuclear energy plant. In particular it is aimed at improved corrosion properties of the alloy with respect to the corrosion properties of the above-mentioned alloys according to the prior art.

This purpose is achieved by means of an alloy of the kind initially defined, which alloy is characterised in that it comprises 0.5-0.85 percentage by weight Sn. This choice of Sn-content stands in opposition to that which, according to the prior art, is a preferred interval for the Sn-content. The applicant has however found that improved corrosion properties, in particular in the environment which is the case in the area of the reactor core of a nuclear energy plant, may be achieved in the zirconium-based alloy by a careful choice of the Sn-content within the defined interval.

According to a preferred embodiment of the alloy, the content of Sn in the alloy is larger than or equal to 0.65 percentage by weight. A preferred interval for the Sn-content should thus be 0.65-0.85 percentage by weight with the purpose of achieving as good corrosion properties in the alloy as possible under the otherwise given conditions.

According to a further preferred embodiment, the alloy comprises up to 0.2 percentage by weight Ni. Thereby secondary phase particles containing Zr, Ni and Fe may be obtained in the alloy. Such secondary phase particles

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contribute to improved corrosion properties of the alloy and have good stability under neutron radiation.

According to a further preferred embodiment, the alloy comprises up to 0.6 percentage by weight Cr, which is more the maximum 0.2 percentage by weight previously been recommended with respect to the formation of binary intermetallic compounds of Cr and Zr. With remaining composition which the alloy according invention has, a content of up to 0.6 percentage by weight may however be permitted in order to improve corrosion properties of the alloy, without the alloy thereby obtaining considerably worse mechanical properties, such as a deteriorated tensile strength. Unlike the prior art, the present invention thus suggests a zirconium-based alloy with a Cr-content above 0.2 percentage by weight, up to 0.6 percentage by weight.

According to a further preferred embodiment, the total content of Nb and Sn is larger than or equal to 1.15 percentage by weight. Such a total content of Nb and Sn contributes to improved mechanical properties of the alloy.

Which requirements on mechanical properties and corrosion properties that finally are demanded on the alloy depend on in which application the alloy finally is to be used. According to a preferred embodiment of the invention, the alloy constitutes at least a part of a component in a nuclear energy plant. The component is preferably arranged in the area of the reactor core and constitutes, according to a further preferred embodiment, a part of a fuel assembly. In such an application high requirements will at least be demanded on the corrosion properties of the alloy. Depending on to which extent the component has a supporting function, specific requirements will also be demanded on the mechanical properties of the alloy. An alloy of the kind

which is suggested by the invention is in particular suitable to constitute at least a part of a cladding tube, a spacer or a box.

A further purpose of the invention is to provide a component in a nuclear energy plant, which component in particular has satisfactory corrosion properties with respect to the specific conditions which may be assumed to be the case in the nuclear energy plant, in particular in the area of the core of the same, where the component is subjected to an increased radiation of the fast neutron kind, in a corrosive environment, e.g. surrounded by a corrosive medium, such as water.

This purpose is achieved by means of a component of the initially defined kind, which comprises an alloy according to the invention.

According to a preferred embodiment, the component constitutes a part of a fuel assembly, i.e. it is arranged 20 the area of the reactor core. Thereby requirements are demanded on its corrosion properties in the environment of increased radiation and corrosive media which it is subjected to. The choice of a zirconium-base alloy 25 with suitable composition is consequently highly important.

According to a further preferred embodiment, the component defines a cladding tube. Thereby also specific mechanical properties of the component are required, which are fulfilled by the alloy according to the invention.

According to a further preferred embodiment, at least a part of the inner circumference of the cladding tube comprises a layer of a material which is more ductile than the alloy according to the invention. The cladding tube is thereby

made less sensitive to the direct contact with the fuel within these. The risk for crack formation of the cladding tube in areas where it comes into direct contact with and possibly is subjected to wear caused by the fuel is reduced, under the condition that the layer of the more ductile material is arranged in these areas, which preferably is the case. Said layer comprises here a zirconium-based alloy with a total content of alloying materials which does not exceed 0.5 percentage by weight.

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Further advantages with and features of the alloy according to the invention and the component, respectively, will be clear from the following, detailed description.

15 DETAILED DESCRIPTION OF A PREFERRED EMBODIMENT

A component arranged in a nuclear energy plant, more precisely in the area of the reactor core, is subjected to increased radiation of the fast neutron kind in a corrosive environment. The reactor may be a pressure water or a boiling water reactor. The component constitutes a part of the fuel assembly. In this example the component is a cladding tube arranged to contain the reactor fuel.

- 25 The component comprises a zirconium-based alloy which has the following composition:
 - 0.5-0.85 percentage by weight Sn,
 - 0.3-0.6 percentage by weight Fe,
- 30 0-0.6 percentage by weight Cr,
 - 0-0.2 percentage by weight Ni,
 - 0.65-1.6 percentage by weight Nb and the rest zirconium.

The content of Ni is preferably within the interval 0.05-0.2 percentage by weight.

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According to an alternative embodiment the alloy comprises 0.65--0.85 percentage by weight Sn and

0.5-1.6 percentage by weight Nb,

with the remaining elements within the previously mentioned intervals.

The cladding tube may be formed from a solid bar, in the centre of which a hole has been drilled. Furthermore, the component has, in addition to prior annealings in connection with the working of the same, finally been annealed in the β -phase area of the alloy and then been quenched by a β -quenching in the α -phase area of the alloy.

By the annealing in the β -phase area, course structures and other effects of the prior heat treatment history are removed from the alloy. Furthermore, the orientated texture which has been obtained during prior working of the work piece of the tube is removed, whereby different tendencies to growth in different directions of the component, when it is exposed to neutron radiation in the core, are avoided.

The cooling to the α -phase area is so fast that an entity of short α -phase laminae is formed in the prior β -phase grains. Short α -laminae improve the mechanical strength of the alloy.

Furthermore at the quenching from the β -phase area to the α -phase area secondary phase particles of intermetallic compounds, such as $Zr(Nb,Fe)_2$, Zr(Fe,Cr,Nb) and $(Zr,Nb)_3Fe$, are precipitated, which favours good anticorrosive and mechanical properties of the finished alloy and thereby of the component. The quenching speed should thereby be adjusted such that an optimal secondary phase particle distribution and secondary phase average particle size are obtained. The alloy is preferably cooled with a cooling

speed below $100^{\circ}\text{C/second}$, preferably below $50^{\circ}\text{C/second}$ and most preferred in order of magnitude $5-20^{\circ}\text{C/second}$.

When the component, such as here, is a cladding tube, preferably a layer with a lower total content of alloying elements than the remaining alloy is applied on the inner circumference of the cladding tube. The total content of alloying materials in this layer is preferably below 0.5 percentage by weight, wherein the remaining part constitutes 2r. This layer makes the cladding tube more resistant to mechanical influence from the reactor fuel which is arranged in the tube and which physically may rest against and cause tensions in the walls of the cladding tube.

Preferably the alloy according to the invention comprises no essential amount of other materials than those which have been mentioned above. It should however be noted that small amounts of impurities may exist in the alloy. Typical impurities which may exist in zirconium-based alloys are specified in the table below. Furthermore, small amounts of Si and O may exist in the alloy. Typical contents of these materials are also given below:

Table:

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	T						
Element	Al	В	С	Ca	Cd	Cl	CO
Max.ppm	75	0.5	270	30	0 5		
T. Ppill	1 / 3	0.5	12/0	130	10.5	120	120 l

Element	Cu	H	Нf	Mg	Mn	Мо	N
Max.ppm	50	25	100	20	50	50	80

Element	Na	Pb	Si	Ti	U
Max.ppm	20	130	120	50	3.5

Si and O may exist in contents where Si is 50-120 ppm and O is 500-1600 ppm.

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It should be realised that a number of alternative embodiments of the alloy and the component according to the invention will be obvious to a person skilled in the art but still be within the scope of the invention, such as it is defined in the annexed claims.

Claims

- 1. A zirconium-based alloy, suitable for use in a corrosive environment, where it is subjected to increased radiation, wherein the alloy, in addition to zirconium and for zirconium of a reactor quality normal contents of impurities, comprises 0.5-1.6 percentage by weight Nb and 0.3-0.6 percentage by weight Fe, characterised in that it comprises 0.5-0.85 percentage by weight Sn.
 - 2. A zirconium-based alloy according to claim 1, characterised in that the content of Sn in the alloy is larger than or equal to 0.65 percentage by weight.
 - 3. A zirconium-based alloy according to claim 1 or 2, characterised in that it comprises up to 0.2 percentage by weight Ni.
- 4. A zirconium-based alloy according to any one of the claims 1-3, characterised in that it comprises up to 0.6 percentage by weight Cr.
- 5. A zirconium-based alloy according to any one of the claims 1-4, characterised in that the total content of Nb and Sn is larger than or equal to 1.15 percentage by weight.
- 6. A zirconium-based alloy according to any one of the claims 1-5, characterised in that the alloy constitutes at least a part of a component in a nuclear energy plant.
 - 7. A zirconium-based alloy according to claim 6, characterised in that said component constitutes a part of a fuel assembly.

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- 8. A component in a nuclear energy plant, <u>characterised in</u> that it comprises an alloy according to any one of the claims 1-5.
- 9. A component according to claim 8, <u>characterised in that</u> it constitutes a part of a fuel assembly.
 - 10. A component according to claim 8 or 9, characterised in that it defines a cladding tube for nuclear fuel.
- 11. A component according to claim 10, characterised in that at least a part of the inner circumference of the component comprises a layer of a material which is more ductile than said alloy.
- 12. A component according to claim 11, characterised in that said layer comprises a zirconium-based alloy with a total content of alloying elements which does not exceed 0.5 percentage by weight.





International application No.

PCT/SE 99/02300

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A. CLASSIFIC	CATION OF SUBJECT MATTER			
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Zirkoniumbaserad legering och komponent i en kärnenergianläggning

10 UPPFINNINGENS BAKGRUND OCH TIDIGARE TEKNIK

Föreliggande uppfinning avser en zirkoniumbaserad legering, lämpad för användning i en korrosiv miljö där den är föremål för förhöjd strålning och innefattande 0,5-1,6 viktsprocent Nb och 0,3-0,6 viktsprocent Fe. Uppfinningen avser dessutom en komponent i en kärnenergianläggning, vilken innefattar en legering av det nämnda slaget.

Enligt tidigare teknik är det känt att i en kärnenergianläggning anordna en komponent som innefattar en zirkoniumbaserad legering av det ovan nämnda slaget. En sådan legering har fördelen att uppfylla de krav som ställs på såväl mekaniska egenskaper som korrosionsegenskaper hos ett material som i en korrosiv miljö är föremål för en förhöjd strålning, i synnerhet neutronstrålning av typen snabba neutroner.

Tack vare dess relativt höga Fe-innehåll är det möjligt att genom lämplig värmebehandling, innefattande glödgning och snabbkylning, erhålla sekundärfaspartiklar bestående av Zr, Fe och Nb hos en matris av α -fas hos den zirkoniumbaserade legeringen. Genom lämpligt val av värmebehandlingsvariablerna tid och temperatur är det dessutom, med givna halter av de ingående legeringsämnena Nb och Fe, möjligt att styra storleken på och fördelningen av sekundärfaspartiklarna. Sekundärfaspartiklarna kan ha en positiv effekt på legeringens korrosionshärdighet. Det är därför viktigt att optimera fördelningen av och storleken på de förekommande sekundärfaspartiklarna. Det är därvid av yttersta vikt

att finna en lämplig sammansättning av de i legeringen ingående legeringselementen.

Skriften US 5,560,790 beskriver en zirkoniumbaserad legering som innefattar 0,5-1,5 viktsprocent Nb, 0,9-1,5 viktsprocent Sn och 0,3-0,6 viktsprocent Fe. Dessutom innehåller denna legering 0,005-0,2 viktsprocent Cr, 0,005-0,04 viktsprocent C, 0,05-0,15 viktsprocent O, 0,005-0,15 viktsprocent Si och resten Zr. Därigenom uppnås en mikrostruktur hos materialet som inbegriper partiklar av typen $Zr(Nb,Fe)_2$, Zr(Nb,Cr,Fe) och $(Zr,Nb)_3Fe$. Dessa sekundärfaspartiklar förlänar materialet goda korrosionsegenskaper och goda mekaniska egenskaper. Tack vare den höga Fehalten undviks utskiljningar av β -Nb-fas, vilka skulle ha en negativ inverkan på materialets motståndskraft mot lokala korrosionsangrepp.

Sn sägs ha hög löslighet i α -fasen och kommer därför, då det är närvarande i den givna mängden, att vara inlöst i α -fasen och bidra till förbättrade korrosionsegenskaper och mekaniska egenskaper hos denna. Det framhålls att ett alltför lågt innehåll av Sn (under 0,9 viktsprocent) hos materialet påverkar brotthållfastheten både på lång och kort sikt hos detta. Dessutom undertrycker ett sådant lågt Sn-innehåll i mindre utsträckning en negativ effekt av eventuell kväveinblandning på materialets korrosionshållfasthet. Ett Sn-innehåll över 1,5 viktsprocent påverkar materialets mottaglighet för bearbetning och i synnerhet kallbearbetning.

Det nämns att Si och C bidrar till att reducera storleken på par-30 tiklar och tillföra strukturhomogenitet hos materialet.

Syre sägs bidra till en finare struktur hos materialet och används även som ett medel för att förstärka materialet genom den fasta lösningen, en så kallad "solid solution strengthener".

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Nb sägs bidra till hållfasthetsegenskaperna hos Zr och ökar legeringens korrosionshållfasthet genom att bilda sekundärfaspartiklar tillsammans med Zr och Fe.

Det konstateras vidare att med ett Nb-innehåll under 0,5 viktsprocent hos materialet, ett Fe-innehåll under 0,3 viktsprocent och ett Cr-innehåll under 0,005 viktsprocent, är den totala andelen av sekundärfaspartiklar av det ovan nämnda slaget i α-zirkoniummatrisen hos slutprodukten väsentligt lägre än 60 volymprocent av den totala mängden av järnhaltiga sekundärfaspartiklar, vilket resulterar i att korrosionshållfastheten hos materialet påverkas negativt. Med ett Nb-innehåll över 1,5 viktsprocent, bildas ett stort antal stora partiklar av β-Nb-fas i materialet, vilket också reducerar dettas korrosionsresistans.

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Det nämns också att ett Cr-innehåll över 0,2 viktsprocent kan resultera i bildande av binära intermetalliska föreningar av Zr-Cr, vilket har motsatt, d.v.s. negativ inverkan på bearbetbarheten och brotthållfastheten hos materialet.

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SAMMANFATTNING AV UPPFINNINGEN

Ett syfte med den föreliggande uppfinningen är att tillhandahålla en zirkoniumbaserad legering med en sådan sammansättning att fördelningen av och storleken på sekundärfaspartiklar i legeringen, typen av sekundärfaspartiklar och innehållet av olika legeringselement i legeringens α-fas är sådana att legeringen är optimerad med hänsyn till såväl fysikaliska och mekaniska egenskaper som korrosionsegenskaper. I synnerhet skall dessa egenskaper vara optimerade med hänsyn till en tillämpning där legeringen är föremål för förhöjd strålning av typen snabba neutroner i en korrosiv miljö, såsom i reaktorhärden hos en kärnenergianläggning. I synnerhet eftersträvas förbättrade korrosionsegenskaper hos legeringen i förhållande till korrosionsegenskaperna hos de ovan nämnda legeringarna enligt tidigare teknik.

Detta syfte uppnås medelst en legering av det inledningsvis definierade slaget, vilken är kännetecknad av att den innefattar 0,5-0,85 viktsprocent Sn. Detta val av Sn-innehåll står i motsägelse till vad som, enligt tidigare teknik, är ett föredraget intervall för Sn-innehållet. Sökanden har emellertid kunnat konstatera att förstrade korrosionsegenskaper, i synnerhet i den miljö som uppbättrade korrosionsegenskaper, i synnerhet i den miljö som upptättrader i området av reaktorhärden hos en kärnenergianläggning, träder i området av reaktorhärden hos en kärnenergianläggning, omsorgsfullt val av Sn-innehåll inom det definierade intervallet.

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Enligt ett föredraget utförande av legeringen är innehållet av Sn i legeringen större än eller lika med 0,65 viktsprocent. Ett föredraget intervall för Sn-innehållet torde sålunda vara 0,65-0,85 viktsprocent i syfte att uppnå så goda korrosionsegenskaper hos legeringen som möjligt under de i övrigt givna förutsättningarna.

Enligt ytterligare ett föredraget utförande innefattar legeringen upp till 0,2 viktsprocent Ni. Därigenom kan sekundärfaspartiklar innehållande Zr, Ni och Fe erhållas i legeringen. Sådana sekundärfaspartiklar bidrar till förbättrade korrosionsegenskaper hos legeringen och har god stabilitet under neutronbestrålning.

Enligt ytterligare ett föredraget utförande innefattar legeringen upp till 0,6 viktsprocent Cr, vilket är mer än de maximala 0,2 viktsprocent som tidigare rekommenderats med hänsyn till bildviktsprocent som tidigare rekommenderats med hänsyn till bildviktsprocent av binära intermetalliska föreningar av Cr och Zr. Med den ammansättning som den uppfinningsenliga legeringen i övrigt uppvisar kan ett innehåll av upp till 0,6 viktsprocent Cr emellertid uppvisar kan ett innehåll av upp till 0,6 viktsprocent Cr emellertid uppvisar för att förbättra korrosionsegenskaperna hos legeringen, tillåtas för att förbättra korrosionsegenskaperna hos legeringen, utan att legeringen därvid erhåller remarkabelt försämrade metaniska egenskaper, såsom försämrad brotthållfasthet. Till skillkaniska egenskaper, såsom försämrad den föreliggande uppnad från tidigare teknik föreslår sålunda den föreliggande uppfinningen en zirkoniumbaserad legering med ett Cr-innehåll över 0,2 viktsprocent, ända upp till 0,6 viktsprocent.

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Enligt ytterligare ett föredraget utförande är det totala innehållet av Nb och Sn större än eller lika med 1,15 viktsprocent. Ett så-

dant totalt innehåll av Nb och Sn bidrar till förbättrade mekaniska egenskaper hos legeringen.

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Vilka krav på mekaniska egenskaper och korrosionsegenskaper som slutligen ställs på legeringen beror av i vilken applikation legeringen till sist skall användas. Enligt ett föredraget utförande av uppfinningen bildar legeringen åtminstone en del av en komponent i en kärnenergianläggning. Komponenten är företrädesvis anordnad i området av reaktorhärden och bildar, enligt ett ytterligare föredraget utförande, del av en bränslepatron. I en sådan applikation kommer stora krav att åtminstone ställas på legeringens korrosionsegenskaper. Beroende av i vilken utsträckning komponenten har en bärande funktion kommer också specifika krav att ställas på legeringens mekaniska egenskaper. En legering av det slag som föreslås av uppfinningen är i synnerhet lämpad att utgöra åtminstone en del av ett kapslingsrör, en spridare eller en box.

Ett ytterligare syfte med uppfinningen är att tillhandahålla en komponent i en kärnenergianläggning, vilken komponent i synnerhet uppvisar tillfredsställande korrosionsegenskaper med hänsyn till de specifika förhållanden som kan antas föreligga i kärnenergianläggningen, i synnerhet i området av dennas härd, där komponenten är föremål för förhöjd strålning av typen snabba neutroner, i en korrosiv miljö, t ex omgiven av ett korrosivt medium, såsom vatten.

Detta syfte uppnås medelst en komponent av det inledningsvis definierade slaget, vilken innefattar en legering av det uppfinningsenliga slaget.

Enligt ett föredraget utförande bildar komponenten del av en bränslepatron, d.v.s den är anordnad i området av reaktorhärden. Därvid ställs speciella krav på dess korrosionsegenskaper i den miljö av förhöjd strålning och korrosiva media som den är föremål för. Valet av en zirkoniumbaserad legering med lämplig sammansättning är följaktligen av yttersta vikt.

Enligt ytterligare ett föredraget utförande definierar komponenten ett kapslingsrör. Därvid fordras även specifika mekaniska egenskaper hos komponenten, vilka uppfylls av den uppfinningsenliga legeringen.

Enligt ytterligare ett föredraget utförande innefattar åtminstone en del av kapslingsröret inre omfång ett skikt av ett mer duktilt material än den uppfinningsenliga legeringen. Därigenom görs kapslingsröret mindre känsligt för den direkta kontakten med bränslet inuti dessa. Risken för sprickbildning hos kapslingsröret i områden där denna kommer i direkt kontakt med och eventuellt är föremål nötning på grund av bränslet reduceras, under förutsättning att skiktet av det mer duktila materialet är anordnat i dessa områden, vilket företrädesvis är fallet. Nämnda skikt innefattar här en zirkoniumbaserad legering med en total halt av legeringsämnen som icke överstiger 0,5 viktsprocent.

Ytterligare fördelar med och särdrag hos den uppfinningsenliga 20 legeringen respektive komponenten kommer att framgå av den följande, detaljerade beskrivningen.

DETALJERAD BESKRIVNING AV ETT FÖREDRAGET UTFÖRANDE

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En komponent anordnad i en kärnenergianläggning, närmare bestämt i området av reaktorhärden, är föremål för förhöjd strålning av typen snabba neutroner i en korrosiv miljö. Reaktorn kan vara en tryckvatten- eller en kokarvattenreaktor. Komponenten bildar del av bränslepatronen. I detta exempel är komponenten ett kapslingsrör inrättat att inhysa reaktorbränslet.

Komponenten innefattar en zirkoniumbaserad legering vilken har följande sammansättning:

0.5-0.85 viktsprocent Sn,

5 0,3-0,6 viktsprocent Fe,

0-0.6 viktsprocent Cr,

0-0,2 viktsprocent Ni,

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0,65-1,6 viktsprocent Nb och resten zirkonium.

10 Innehållet av Ni ligger företrädesvis i intervallet 0,05-0,2 viktsprocent.

Enligt ett alternativt utförande innefattar legeringen 0,65-0,85 viktsprocent Sn och

15 0,5-1,6 viktsprocent Nb, med övriga element inom de tidigare nämnda intervallen.

Kapslingsröret kan vara bildat utifrån en solid stång, i vars centrum ett hål borrats. Vidare har komponenten, förutom tidigare glödgningar i samband med bearbetningen därav, slutligen glödgats i legeringens β -fasområde och sedan snabbkylts genom en β -släckning till legeringens α -fasområde.

Genom glödgningen i β-fasområdet avlägsnas grova strukturer och andra effekter av tidigare värmebehandlingshistorik ur legeringen. Dessutom avlägsnas den orienterade textur som erhållits vid tidigare bearbetningar av rörämnet, varigenom olika benägenhet till växning i olika riktningar hos komponenten, då denna utsätts för neutronstrålningen i härden, undviks.

Kylningen till α -fasområdet är så snabb att paket av korta α -faslameller bildas i de tidigare β -faskornen. Korta α -lameller gynnar legeringens mekaniska hållfasthet.

Vid snabbkylningen från β-fasområdet till α-fasområdet utskiljs dessutom sekundärfaspartiklar av intermetalliska föreningar, såsom $Zr(Nb,Fe)_2$, Zr(Fe,Cr,Nb) och $(Zr,Nb)_3Fe$, vilka gynnar goda

antikorrosiva och mekaniska egenskaper hos den färdiga legeringen och därmed komponenten. Kylningshastigheten bör därvid anpassas så att en optimal sekundärfaspartikelfördelning och sekundärfaspartikelmedelstorlek erhålls. Legeringen är företrädesvis kyld med en svalningshastighet under 100°C/sekund, företrädesvis under 50°C/sekund och helst i storleksordningen 5-20°C/sekund.

Då komponenten, såsom här, är ett kapslingsrör, är företrädesvis ett skikt med lägre total halt av legeringselement än hos legeringen i övrigt applicerad på kapslingsrörets inneromfång. Den totala halten av legeringsämnen hos detta skikt ligger företrädesvis under 0,5 viktsprocent, varvid återstoden utgörs av Zr. Detta skikt gör kapslingsröret mer motståndskraftigt mot mekanisk påverkan från det reaktorbränsle som är anordnat i röret och som fysiskt kan komma att ligga an mot och orsaka spänningar i kapslingsrörets väggar.

Företrädesvis innefattar legeringen enligt uppfinningen ingen väsentlig mängd av andra ämnen än de som omnämnts ovan. Det ska emellertid noteras att små mängder föroreningar kan finnas i legeringen. Typiska föroreningar som förekommer i zirkoniumbaserade legeringar är specificerade i tabellen nedan. Dessutom kan små mängder av Si och O förekomma i legeringen. Typiska halter av dessa ämnen anges också nedan.

Tabell:

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Element	Al	В	С	Са	Cd	CI	Со
Max.ppm	75	0,5	270	30	0,5	20	20

Element	Cu	Н	Hf	Mg	Mn	Мо	N
Max.ppm	50	25	100	20	50	50	80

Element	Na	Pb	Si	Ti	U
Max.ppm	20	130	120	50	3,5

Si och O förekommer i halter där Si är 50 -120 ppm och O är 500 - 1600 ppm.

Det skall inses att en rad alternativa utföranden av den uppfinningsenliga legeringen och komponenten kommer att vara uppenbara för en fackman inom området men ändock ligga inom ramen för uppfinningen, såsom den är definierad i de bifogade patentkraven.

<u>Krav</u>

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- 1. Zirkoniumbaserad legering, lämpad för användning i en korrosiv miljö, där den är föremål för förhöjd strålning, varvid legeringen, förutom zirkonium och för zirkonium av reaktorkvalitet normala halter av föroreningar, innefattar 0,5-1,6 viktsprocent Nb och 0,3-0,6 viktsprocent Fe, kännetecknad av att den innefattar 0,5-0,85 viktsprocent Sn.
- 10 2. Zirkoniumbaserad legering enligt krav 1, <u>kännetecknad av</u> att innehållet av Sn i legeringen är större än eller lika med 0,65 viktsprocent.
- 3. Zirkoniumbaserad legering enligt krav 1 eller 2, <u>känneteck-</u> 15 <u>nad av</u> att den innefattar upp till 0,2 viktsprocent Ni.
 - 4. Zirkoniumbaserad legering enligt något av kraven 1-3, <u>kännetecknad av</u> att den innefattar upp till 0,6 viktsprocent Cr.
- 20 5. Zirkoniumbaserad legering enligt något av kraven 1-4, <u>kän-netecknad av</u> att det totala innehållet av Nb och Sn är större än eller lika med 1,15 viktsprocent.
- 6. Zirkoniumbaserad legering enligt något av kraven 1-5, <u>kän-</u> 25 <u>netecknad av</u> att legeringen bildar åtminstone en del av en komponent i en kärnenergianläggning.
 - 7. Zirkoniumbaserad legering enligt krav 6, <u>kännetecknad av</u> att nämnda komponent bildar del av en bränslepatron.
 - 8. Komponent i en kärnenergianläggning, <u>kännetecknad av</u> att den innefattar en legering enligt något av kraven 1-5.
- 9. Komponent enligt krav 8, <u>kännetecknad av</u> att den bildar del 35 av en bränslepatron.

- 10. Komponent enligt krav 8 eller 9, <u>kännetecknad av</u> att den definierar ett kapslingsrör för kärnbränsle.
- 11. Komponent enligt krav 10, <u>kännetecknad av</u> att åtminstone 5 en del av dess inneromfång innefattar ett skikt av ett material som är mer duktilt än nämnda legering.
- 12. Komponent enligt krav 11, <u>kännetecknad av</u> att nämnda skikt innefattar en zirkoniumbaserad legering med en total halt av legeringsämnen icke överstigande 0,5 viktsprocent.

Sammandrag

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En zirkoniumbaserad legering, lämpad för användning i en korrosiv miljö, där den är föremål för förhöjd strålning och innefattande 0,5-1,6 viktsprocent Nb och 0,3-0,6 viktsprocent Fe. Legeringen är kännetecknad av att den innefattar 0,5-0,85 viktsprocent Sn.